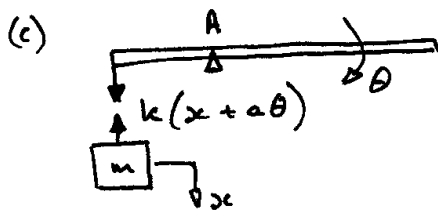


STRUCTURAL VIBRATION 1 SHEET 2

Q1 If you have difficulty with (a) or (b), please go to the next Subject Tutorial.

For (b), note that for springs in PARALLEL, $K = k_1 + k_2 + \dots$

For springs in SERIES, $\frac{1}{K} = \frac{1}{k_1} + \frac{1}{k_2} + \dots$



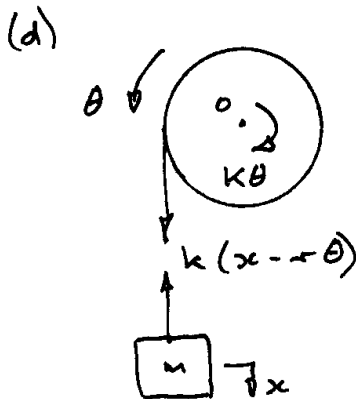
Equations of motion

Bar: $A \cdot \ddot{\theta}$

$$-k(x + a\theta)a = I \ddot{\theta}$$

Mass: $\downarrow \ddot{x}$

$$-k(x + a\theta) = m \ddot{x}$$



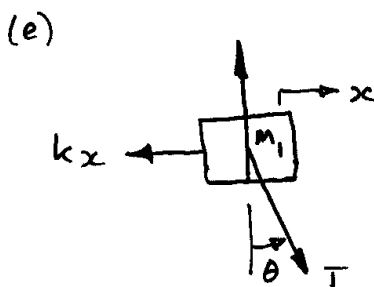
Equations of motion

Disc: $O \cdot \ddot{\theta}$

$$k(x - r\theta)r - k\theta = I \ddot{\theta}$$

Mass: $\downarrow \ddot{x}$

$$-k(x - r\theta) = m \ddot{x}$$



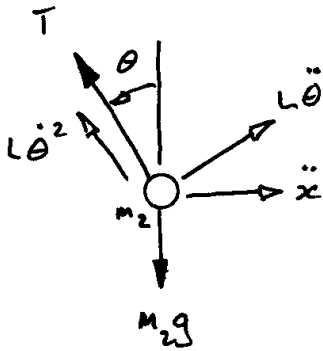
Equation of motion

Mass m_1 : $\ddot{x} \rightarrow$

$$T \sin \theta - kx = m_1 \ddot{x}$$

For small θ ,

$$T\theta - kx = m_1 \ddot{x} \quad (1)$$



Linear equations of motion involve the absolute acceleration of the centre of mass. Here, mass m_2 has components of $L\dot{\theta}^2$ and $L\ddot{\theta}$ relative to mass m_1 , which itself has an absolute acceleration \ddot{x} . Equations for horizontal and vertical translation are

$$\begin{aligned} \rightarrow : \quad -T \sin \theta &= m_2 [\ddot{x} + L\ddot{\theta} \cos \theta - L\dot{\theta}^2 \sin \theta] \\ \uparrow : \quad T \cos \theta - m_2 g &= m_2 [L\ddot{\theta} \sin \theta + L\dot{\theta}^2 \cos \theta] \end{aligned}$$

For small θ , these become

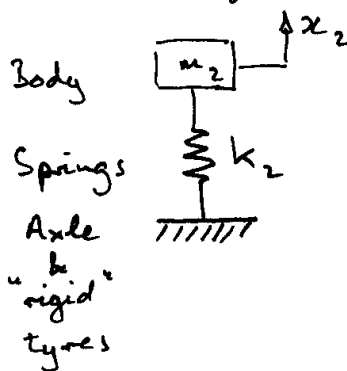
$$-T\theta = m_2 [\ddot{x} + L\ddot{\theta} - L\dot{\theta}^2 \theta] \quad (2)$$

$$T - m_2 g = m_2 [L\ddot{\theta} \theta + L\dot{\theta}^2] \quad (3)$$

Neglect the products of small quantities so that

$\dot{\theta}^2 \theta = \ddot{\theta} \theta = \dot{\theta}^2 = 0$ and then eliminate T from equations (1) - (3).

2(a) 1 degree-of-freedom model



$$-k_2 x_2 = m_2 \ddot{x}_2$$

$$\text{or } m_2 \ddot{x}_2 + k_2 x_2 = 0$$

$$\omega_n = \sqrt{\frac{k_2}{m_2}} = \sqrt{\frac{40,000}{350}} = 1.70 \text{ Hz}$$

2(b) 2 degree-of-freedom model - see lecture notes

3. Equations of motion derived in Q1(a)

Put $x_i = X_i \cos \omega t$, etc and substitute for mass and stiffness values

$$\begin{bmatrix} 10^4 - 5\omega^2 & -10^4 & 0 \\ -10^4 & 4 \times 10^4 - 5\omega^2 & -3 \times 10^4 \\ 0 & -3 \times 10^4 & 3 \times 10^4 - 20\omega^2 \end{bmatrix} \begin{Bmatrix} X_1 \\ X_2 \\ X_3 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 0 \end{Bmatrix}$$

Put $\phi = \frac{5\omega^2}{10^4}$ to simplify subsequent algebra. Hence

$$\begin{bmatrix} 1 - \phi & -1 & 0 \\ -1 & 4 - \phi & -3 \\ 0 & -3 & 3 - 2\phi \end{bmatrix} \begin{Bmatrix} X_1 \\ X_2 \\ X_3 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 0 \end{Bmatrix} \quad \begin{array}{l} \text{(i)} \\ \text{(ii)} \\ \text{(iii)} \end{array}$$

The frequency equation is

$$2\phi^3 - 13\phi^2 + 12\phi = 0$$

Roots give the natural frequencies.

Mode shapes

From (i), $(1 - \phi)X_1 - X_2 = 0 \quad \therefore \begin{Bmatrix} X_1 \\ X_2 \end{Bmatrix} = \begin{Bmatrix} 1/(1 - \phi) \\ 1 \end{Bmatrix}$

From (iii), $-3X_2 + (3 - 2\phi)X_3 = 0 \quad \therefore \begin{Bmatrix} X_3 \\ X_2 \end{Bmatrix} = \begin{Bmatrix} 3/(3 - 2\phi) \\ 1 \end{Bmatrix}$

Combining the two, we get,

$$\begin{Bmatrix} X_1 \\ X_2 \\ X_3 \end{Bmatrix} = \begin{Bmatrix} 1/(1 - \phi) \\ 1 \\ 3/(3 - 2\phi) \end{Bmatrix}$$